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The different impacts of SO₂ and SO₃ on Cu/zeolite SCR catalysts

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ABSTRACT

The different impacts of SO_2 and SO_3 on Cu/zeolite SCR catalysts were investigated by SCR performance tests and multiple characterization techniques including temperature programmed desorption (TPD), X-ray photoelectron spectroscopy (XPS) and X-ray absorption fine structure (XAFS). The results indicate that a larger amount of highly dispersed $CuSO_4$ formed in the zeolite catalysts (Z-CuSO₄) upon SO_3 poisoning, explaining the much more significant deactivation of the Cu/zeolite catalysts that were exposed to SO_3 compared to poisoning by SO_2 . This paper provides the first demonstration that active sites of Cu/zeolite SCR catalysts involved in the storage and removal of sulfur can react with SO_2 and SO_3 in very different ways. In particular, the significant differences in the extent of sulfur uptake account for the considerably different impacts of SO_2 and SO_3 poisoning on the performance of SO_2 catalysts.

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1. Introduction

Cu/zeolite catalysts for the selective catalytic reduction (SCR) of NOx with aqueous urea have high de-NOx activity and superior thermal durability. As such, these catalysts are among the leading candidates for the treatment of NOx emissions for diesel vehicles required to meet Federal Tier 2 and California LEVII emission standards [1–4]. It is known that Cu/zeolite SCR catalysts are especially sensitive to sulfur poisoning [5–10]. The SCR performance of sulfur poisoned Cu/zeolite catalysts is reduced to a significant extent, although the catalysts can be regenerated by decomposing the sulfates (deSOx) at high temperatures under lean conditions. Sulfur poisoning directly impacts the overall SCR performance and durability of Cu/zeolite SCR catalysts [4–6]. This problem will remain as long as sulfur is present in the fuels and engine oils, even at the "ultra low" sulfur levels (containing less than 15 ppm sulfur) applied in the future.

Most studies on sulfur poisoning of transition metal/zeolite SCR catalysts have used SO_2 as the poisoning agent [7–10]. Insofar as diesel oxidation catalysts (DOCs) will be employed upstream of the SCR catalysts for most applications, it is likely that at least a portion of the SO_2 will be oxidized into SO_3 . Our recent studies [5] showed that the NOx activity of Cu/zeolites is significantly reduced for samples poisoned by SO_3 vs. those poisoned by SO_2 . The results indicated that sulfur poisoning by SO_2 and SO_3 are not equivalent, with different poisoning mechanisms and impacts. Thus, this study

points to an important sulfur poisoning concern for systems with DOCs in front of SCR catalysts in diesel engine applications. To understand the different impacts of SO₂ and SO₃ on Cu/zeolite SCR catalysts, lab aged Cu/zeolite SCR catalysts were assessed by performance tests in simulated diesel exhaust gas in a lab flow reactor. The focus of this paper is to investigate and understand correlations between activity deterioration of Cu/zeolite SCR catalysts and the changes of Cu active sites after being poisoned by SO₂ and SO₃. The poisoned and regenerated (deSOxed) catalysts were characterized by X-ray photoelectron spectroscopy (XPS), temperature programmed desorption (TPD), and X-ray absorption fine structure (Cu K-edge XAFS) to develop an understanding of sulfur poisoning. The results of this study provide, for the first time, insight into the different poisoning mechanisms between SO2 and SO₃, and also provide valuable information on the durability of SCR catalysts for lean-burn vehicle applications.

2. Experimental

The Cu/zeolite SCR catalysts used in this study were: CatA which was a fully formulated cordierite monolith with Cu/zeolite washcoat from a catalyst supplier, and CatB, a beta zeolite-based Cu/zeolite SCR catalyst that we synthesized. The CatB catalyst was prepared by ion exchange of a NH⁴⁺-BEA zeolite with Si/Al₂ = 25, obtained from Zeolyst International (CP814E), using aqueous Cu(NO₃)₂ solutions. These solutions contained total Cu²⁺ ion concentrations \sim 250% of the zeolite cation sites. Following the ion exchange, the samples were thoroughly washed with distilled water and then dried at 120 °C in air. Ion-exchange processes were repeated 2 times to ensure 100% exchange levels. The dried CatB

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was activated at 500 °C for 2 h under flowing zero air before any catalyst characterization or performance measurement. For proprietary reasons, details of CatA cannot be given in this paper. While the type of zeolite and Cu loading in CatA may well be different than CatB, both catalysts were designed for transient diesel engine applications, and the test results showed that they both had similar deactivation behavior with respect to SO_2 and SO_3 aging. Moreover, characterization (e.g., XPS) of both catalysts studied here showed similar results after poisoning with SO_2 and SO_3 , corroborating the conclusions made here.

The CatA monolith samples were cored to sizes of 1 in. diameter by 1 in. long and were aged and tested using a laboratory flow reactor at a space velocity of $30,000\,h^{-1}$. Before any sulfur poisoning, the samples were hydrothermally aged with $14\%~O_2$, $5\%~CO_2$, $4.5\%~H_2O$, and N_2 balance, at $670~^{\circ}C$ for 20~h. Then, the samples were exposed to $40~ppm~SO_2~or~SO_3$ in a gas mixture containing $14\%~O_2$, $5\%~CO_2$, $4.5\%~H_2O$, and N_2 balance at 200,300, and $400~^{\circ}C$ for 1.5~h. The total sulfur exposures corresponded to 500~sulfur-equivalent miles with 350~ppm~sulfur~fuel, a relatively high sulfur fuel currently available in the US.

To remove sulfur (deSOx), the sulfated samples were first heated and stabilized in the reactor at 170 °C in 14% O₂, 5% CO₂, and 4.5% H₂O and N₂ balance. Then, the stored sulfur was removed by heating the catalysts in the same gas mixture from 170 to 770 °C at a rate of 5 °C/min. The NOx performance was measured before the sulfur poisoning (Test1), after the sulfur poisoning (Test2), and after the deSOx (Test3). Steady state NOx activities of samples were measured from 130 to 340 °C in a flow reactor connected to an FTIR instrument from MIDAC Corporation with a heated sample cell for gas analysis. The SCR evaluation was stopped at 340 °C to prevent decomposition of any sulfates on the catalyst surface that were generated during the sulfur aging. For the steady state SCR activity measurements, simulated diesel exhaust gas (composition shown in Table 1) was flowed through the sample core.

Selected SO_2 and SO_3 poisoned CatA and CatB samples were characterized by XPS and Cu K-edge XAFS. XPS experiments were carried out for samples aged at $200\,^{\circ}\text{C}$ with SO_2 and SO_3 . For 27 mm (1 in.) long CatA monolith core samples, 5 points, separated by a distance of 6 mm, were analyzed in the analysis chamber of a Physical Electronics Instruments Quantum 2000 using Al K α X-rays and a pass energy of 71 eV. The position and intensity of the Al 2s peak at 119.2 eV were used as references. CatB samples were analyzed with XPS in the powder form, after the treatment with SO_2 or SO_3 .

Cu K-edge XAFS measurements were carried out for CatB samples at beam line X19A of the National Synchrotron Light Source (NSLS) at Brookhaven National Laboratory. The X19A beamline used to collect the Cu K-edge XANES data is equipped with a double-crystal Si(1 1 1) monochromator. Fluorescence measurements were performed using a passivated implanted planar silicon (PIPS) detector (Canberra Industries, CT). The beam path from the incident ion chamber to the sample chamber was purged with He gas. A small amount of well-mixed sample was evenly spread over double-sided tape. The X-ray energy for the K-edge of Cu metal was used for calibrating the energy scale. The statistical noise at X19A is better than 0.001%. Structural parameters were obtained through curve fitting using Athena and Artemis programs packaged in the theoretical Feff8 computer code, IFEFFIT 8.0.

Table 1Composition of the simulated diesel exhaust gas mixture used for SCR activity measurements.

Component	O_2	H_2O	CO_2	NO	NH ₃	N_2
Concentration	14%	4.5%	5%	350 ppm	350 ppm	Balance

3. Results and discussion

3.1. The impacts of SO_2 and SO_3 poisoning on Cu/zeolite SCR catalyst activity

Previous studies [6] have shown that the impact of sulfur was mainly on the low temperature NOx activity for Cu-based zeolite SCR catalysts, and that stored sulfur starts to release from the catalyst around 350 °C under lean deSOx conditions. As such, the measurements of NOx performance of sulfur-aged SCR catalysts were limited to temperatures below 340 °C in this study. The NOx activities for CatA samples before and after sulfur poisoning by SO₂ at 200, 300, and 400 °C are shown in Fig. 1. The NOx activity of Cu/ zeolite SCR catalysts decreased to a relatively small extent after being exposed to 40 ppm SO₂ for 1.5 h regardless of the SO₂ aging temperatures. The lower SO₂ aging temperature resulted in higher NOx activity decreases: the NOx activities performed at 178 °C decreased by 33%; by 21% for the sample aged at 300 °C, and only by 8% for the sample aged at 400 °C. Fig. 2 shows the NOx activity of CatA Cu/zeolite catalysts before and after sulfur poisoning by SO₃ at 200, 300, and 400 °C. The NOx activities were significantly decreased for all samples after being exposed to 40 ppm SO₃ for 1.5 h regardless of the exposure temperatures, with NOx activities of all samples being extremely low at T < 250 °C. The sample aged with SO₃ at lower temperature had better NOx activity between 250 and 340 °C. Notably at a 340 °C test temperature, the NOx activity of the sample aged at 200 °C was close to 100%, while the NOx activity of sample aged at 400 °C showed only 70% conversion.

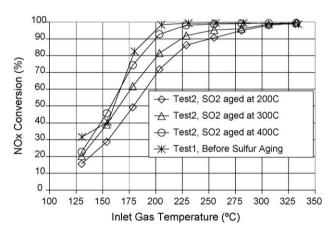


Fig. 1. Steady state NOx conversions for CatA Cu/zeolite SCR catalysts before and after SO_2 aging at 200, 300, and 400 °C.

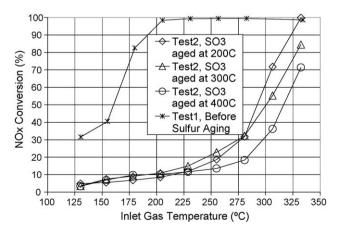


Fig. 2. Steady state NOx conversions for CatA Cu/zeolite SCR catalysts before and after SO_3 aging at 200, 300, and 400 °C.

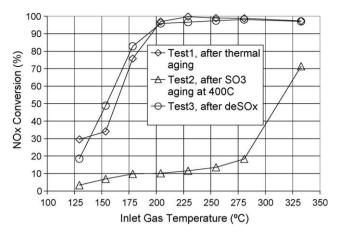


Fig. 3. Steady state NOx conversions for CatA Cu/zeolite SCR catalysts before and after SO_3 aging at 400 °C, and after the deSOx.

Fortunately, NOx activity was restored for all sulfur-aged samples after carrying out a deSOx process, even for catalysts that were significantly deactivated by the SO₃ aging. As an example, Fig. 3 shows the NOx activity of SO₃ aged CatA Cu/ zeolite before the sulfur poisoning (Test1), after the sulfur poisoning by SO₃ at 400 °C (Test2), and after the deSOx (Test3). This figure demonstrates that the NOx activities in Test3 were essentially the same as those in Test1, indicating that CatA regained full SCR function after the deSOx. SO2 was the main sulfur compound released during the deSOx for the samples aged with SO₂ or SO₃. During the deSOx procedure, the amounts of SO₂ released from the SO₃ aged CatA Cu/zeolite SCR catalysts were 5-15 times higher than those from the SO₂ aged samples as shown in Fig. 4. Since the released SO₂ depends on the surface coverage, these results suggest that the samples aged with SO₃ had much higher sulfur coverages compared to those aged with SO₂. In other words, comparing to SO₂, SO₃ tended to remain/ store more on the CatA Cu/zeolite SCR catalysts even though the total sulfur(S) exposures were same for all the samples poisoned by SO₂ and SO₃. (Note that, although the total sulfur(S) exposures were the same for all the samples poisoned by SO₂ and SO₃ before the deSOx, no sulfur measurement was made during this process. As such, we are not able to estimate sulfur coverages before the deSOx.) The results so far indicate that the active sites of Cu/zeolite SCR catalysts involved in sulfur storage and removal react with SO2 and SO3 in very different ways.

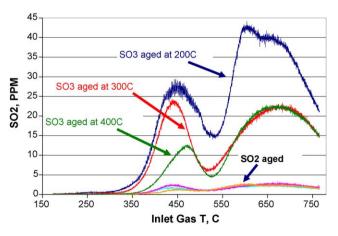


Fig. 4. Released SO_2 from CatA Cu/zeolite SCR catalysts aged with SO_2 or SO_3 observed during the deSOx process.

3.2. The characterizations of SO₂ and SO₃ poisoned Cu/zeolite SCR catalysts

There is little available literature to explain SO_3 poisoning mechanisms of Cu/zeolite SCR catalysts. Ramachandran et al. [7] observed that V–ZSM-5 catalysts exhibit stable activity for NO reduction in the presence of H_2O and SO_2 but rapidly deactivate in the presence of $10~\rm ppm~SO_3$. These authors attributed the possible SO_3 deactivation to the formation of ammonium (bi)sulfate when both NH_3 and SO_3 are present. However, there was no NH_3 during the aging in this study and, therefore, it is not likely that ammonium (bi)sulfate formation can explain the results presented here.

In order to obtain the information on the oxidation state and amount of sulfur species, we applied X-ray photoelectron spectroscopy (XPS) for the CatA samples treated at 200 °C with SO₂ and SO₃. For the 27 mm (1 in.) long monolith samples, 5 points were analyzed separated by a distance of 6 mm, allowing us to determine the spatial distribution along the monolith zaxis. Spectra of both samples contain a single peak at 169 eV, indicating that only sulfates (SO₄²⁻) are formed by the interaction with either SO₂ or SO₃. However, there was a drastic difference in the amount of sulfate species between the samples treated with SO₂ or SO₃. As shown in Fig. 5, the sample treated with SO₃ clearly had larger amounts of sulfur, especially up to 13 mm from the inlet, followed by a significant decrease thereafter. We suggest that sulfate saturates the catalyst from the inlet, gradually moving toward the outlet. In contrast, the sample treated with SO₂ had considerably smaller amount of sulfur in the inlet and along the monolith. The summed amounts of sulfur along the monolith indicates that the sample treated with SO₃ contained at least 5 times larger concentrations than the one treated with SO₂, which points to the relative ease of sulfate formation by reaction with SO3. XPS results on the samples after the desulfation (deSOx) showed essentially no sulfur remained on the surface of the catalyst (not shown). This result implies that all sulfates are desorbed as a result of thermal desorption during the deSOx, as evidenced also by the larger desorption of SO₂ during the deSOx for the sample treated with SO₃ than one treated with SO₂, and the full recovery of the activity as shown in Fig. 3.

In addition to CatA samples, we also performed similar XPS analyses of the CatB samples. As shown in Fig. 6, the samples

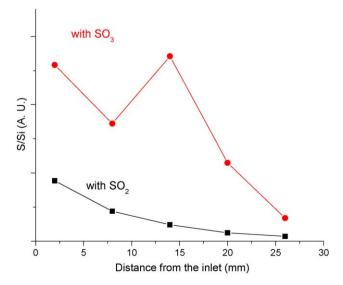


Fig. 5. Distribution of sulfur, plotted as normalized S/Si ratios, as a function of distance from the inlet of the monolith-type CatA sample.

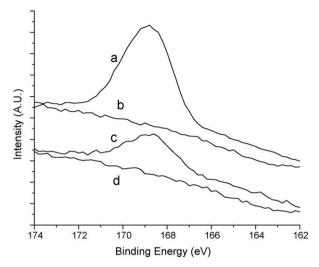


Fig. 6. S 2p XPS spectra for various CatB samples: (a) following SO_3 treatment at 200 °C and (b) after DeSOx; and (c) following SO_3 treatment at 300 °C and (d) after deSOx.

sulfated with SO_3 contained measurable amounts of sulfate on the surface, while the one sulfated with SO_2 (spectrum not shown) did not have any observable sulfur species. Note that the sample sulfated with SO_3 at $200\,^{\circ}\text{C}$ has a larger peak of sulfate than the sulfated sample prepared at $300\,^{\circ}\text{C}$, thus accounting for the relative SO_2 desorption amounts observed during deSOx of CatA samples as shown in Fig. 4. After the deSOx, both samples contained no XPS-observable sulfur species on the surface, again suggesting that the high temperature treatment resulted in complete removal of adsorbed sulfur as SO_2 gas, consistent with the XPS results for CatA.

Finally, we used XANES/EXAFS analyses to investigate properties of the copper species before and after sulfation with SO₃. Fig. 7 shows the Cu K-edge XANES spectra for the CatB samples before and after SO₃ sulfation, as well as the spectra for CuSO₄ as a reference. The XANES spectra between 8975 and 8985 eV were similar for both unsulfated and SO₃ sulfated samples, but quite different from the spectrum of bulk CuSO₄. This suggests that the sulfate formation resulting from SO₃ treatment does not induce any macroscopic changes in the Cu

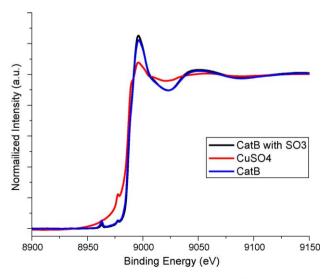


Fig. 7. Cu XANES spectra of ${\rm CuSO_4}$, freshly aged ${\rm CatB}$ (unsulfated) and ${\rm SO_3}$ treated ${\rm CatB}$.

Table 2Summary of XAFS curve fitting for Cu in the CatB sample using Feff7 and FEFFIT^a.

Sample	Pair	CN ^b	r (nm) ^c	$a^2 (pm^2)^d$	AE (eV)
Cu aged CuZ desulfated CuZ sulfated	Cu-0 Cu-0 Cu-0	3.5 ± 0.5 3.4 ± 0.3 3.5 ± 0.3	$\begin{aligned} 0.195 \pm 0.001 \\ 0.195 \pm 0.001 \\ 0.195 \pm 0.001 \end{aligned}$	57 ± 11 54 ± 8 46 ± 6	$-3.4 \pm 2.1 \\ -3.4 \pm 1.4 \\ -3.5 \pm 1.2$

- ^a The many body reduction factor was fixed to 0.9. The fitting ranges were 20–139 nm⁻¹ for Δk and 0.100–0.300 nm for Δr , respectively. The restraint was applied to the Debye–Waller factor for the multiple scattering.
- ^b Coordination number.
- ^c Coordination distance.
- ^d The Debye–Waller factor accounting thermal and statistical vibration.

species; in other words, Cu remains in a highly dispersed state as its initial ion-exchange locations. This behavior also is similar to that observed by Hamada et al. [11] for a Cu–ZSM-5 catalyst after SO_2/O_2 treatment.

The EXAFS region of the data shown in Fig. 7 was analyzed to get more specific information about the coordination of Cu after SO₃ sulfation and freshly aged (unsulfated). Table 2 summarizes the EXAFS curve fitting for these samples. The freshly aged CatB sample contains Cu-O bonds with a coordination number of 3.5 and bond distance of 0.195 nm, consistent with previous EXAFS analyses of a fresh Cu-BEA sample [12]. After treatment with SO₃, CatB maintains similar Cu-O bond coordination, indicating that sulfate species bound to Cu do not induce changes in the local structure of Cu within the zeolite framework. Similarly, subsequent desulfation does not change the Cu-O coordination or bond distance in the CatB catalyst. It is noteworthy that significant Cu-Cu coordination was not observed even after desulfation, suggesting that the copper species in the samples has not sintered. Taken together, these results explain the reversible recovery of activity after a deSOx process at elevated

The above results are consistent with a previous report by Hass and Schneider [13] that used density functional calculations to show that Z-CuSO₄ are the energetically most stable adsorbed SOx species compared to Z-CuSO₃ or Z-CuSO₂. Upon sulfation with SO₃, sulfur exists in a highly dispersed Z-CuSO₄ form (as distinguished from bulk CuSO₄). Furthermore, the lowered affinity of the Cu-zeolite catalysts for SO₂ can be rationalized by these prior calculations.

4. Conclusions

The NOx activity results described here show that SO₃ poisoning causes much more significant deactivation of Cu/ zeolite catalysts than SO₂. XPS data indicate that the sample sulfated with SO₃ contains markedly larger amounts of sulfur, present as sulfates (SO₄²⁻) with an XPS peak at 169 eV, than the one sulfated with SO₂. XANES/EXAFS analyses further demonstrate that sulfate formation does not induce measurable changes in the state of Cu; in other words, Cu remains in a highly dispersed state at zeolite ion-exchange sites as before sulfation with SO₃. In particular, the EXAFS analyses confirm that sulfate formation as a result of SO₃ exposures does not induce changes in the local structure of Cu within the zeolite structure. Thus, we propose that sulfur exists as highly dispersed CuSO₄ in the zeolite (Z-CuSO₄). The calculated lower stability of Z-CuSO₃ and Z-CuSO₂ species [13] may explain the much lower observed levels of sulfate formed following exposures to SO₂ described here. This then explains why SO₃ poisoning causes much more significant deactivation for the Cu/zeolite catalysts than SO₂ poisoning. The results of this paper provide the first direct characterization of differences in the poisoning mechanisms between SO₂ and SO₃, and also provide valuable information for the maintenance of Cu/zeolite SCR catalyst performance for diesel vehicle applications.

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References

- [1] C. Lambert, J. Vanderslice, R. Hammerle, R. Belaire, Application of Urea SCR to Light-Duty Diesel Vehicles, SAE 2001-01-3623.
- [2] C. Lambert, R. Hammerle, R, McGill, M. Khair, C. Sharp, Technical Advantages of Urea SCR for Light-Duty and Heavy-Duty Diesel Vehicle Applications, SAE 2004-01-1292.
- [3] S.J. Schmieg, J.-H. Lee, Evaluation of Supplier Catalyst Formulations for the Selective Catalytic Reduction of NOx with Ammonia, SAE 2005-01-3881.
- [4] G. Cavataio, J. Girard, J. Patterson, C. Montreuil, Y. Cheng, C. Lambert, Laboratory Testing of Urea-SCR Formulations to Meet Tier 2 Bin 5 Emissions, SAE 2007-01-1575.
- [5] Y. Cheng, C. Montreuil, G. Cavataio, C. Lambert, The Effects of SO₂ and SO₃ Poisoning on Cu/Zeolite SCR Catalysts, SAE 2009-01-0898.
- [6] Y. Cheng, C. Montreuil, G. Cavataio, C. Lambert, Sulfur Tolerance and DeSOx Studies on Diesel SCR Catalysts, SAE 2008-01-1023.
- [7] B. Ramachandran, R.G. Herman, S. Choi, H.G. Stenger, C.E. Lyman, J.W. Sale, Catal. Today 55 (2000) 281.
- [8] M. Shibata, H. Nagata, S. Takeshima, K. Hoshino, A Study of Engine Oil Composition Effects on Zeolite-type SCR Catalyst Durability, SAE 2007-01-1924.
- [9] I.S. Nam, S.T. Choo, D.J. Koh, Y.G. Kim, Catal. Today 38 (1997) 181.
- [10] A. Palomares, J. Prato, A. Corma, Catal. Today 75 (2002) 367-371.
- [11] H. Hamada, N. Matsubayashi, H. Shimada, Y. Kintaichi, T. Ito, A. Nishijima, Catal. Lett. 5 (1990) 189.
- [12] S. Dzwigaj, J. Janas, J. Gurgul, R.P. Socha, T. Shishido, M. Che, Appl. Catal. B 85 (2009) 131.
- [13] K.C. Hass, W.F. Schneider, Phys. Chem. Chem. Phys. 1 (1999) 639.